Part I. Write your answer in the space provided. Use equations and sketches in addition to words (as needed).

a. Give a qualitative definition of porosity. 1.

The fraction of a roch that is occupied by vaids or proces - an intensive property of a roch that is a measure of its flind Storage capacity Give a quantitative definition of porosity (\$\phi\$). Define all terms.

 $\phi = \frac{V_P}{V_D} = 1 - \frac{V_m}{V_D}$ where V_m is matrix volume Vh is buth valume

c. Give three examples of geologic processes in the development of induced porosity.

- grain dersolution in sand stones or carbonates - vugs and solution channels in carbonates - fracture development in some sandstones, carbonates and shales a. Give a qualitative definition of permeability.

2.

an intension property of a rock-flerick system that is a measure of its flerick conductionity or to capacity to transmit flerick

b. Give a quantitative definition of permeability (k). Define all terms.

b. Give a quantitative definition of permeability (k). Define all terms. $k = \frac{g L}{A L P}$ Where wis nessort, (cp)

L is length of flow path (and)

(d = \frac{cp.cm^2}{atn-s})

c. Give three sources for permeability determination. Therefore left path (atn)

along flaw path (atn)

- Core analysis - well test analysis - production data log data

3. a. Give a qualitative definition of isothermal compressibility. The fractional change i valume caused by a change in pressure at constant temperature_ an intensive property -- always positive. b. Give a quantitative definition of isothermal compressibility (c). Define all terms.

c. Explain the term, "hysteresis".

- The lagging of an effect behind its cause Vp Shysteress in pore valune of path dependence of path dependence of path dependence of which we make a gualitative definition of non-Darcy flow.

my flaw which is not laminar and Kence cannot be modeled by the Darcy egn.

b. Give two examples of non-Darcy flow.

-gas slippage - inertial effects and turbulence

c. Show that the dimension of the non-Darcy flow coefficient is $[L]^{-1}$.

Frakkeine eg: $-\frac{df}{di}\left[\frac{P}{I}\right] \Rightarrow \left[p\left(\frac{gg}{A}\right)^{2}\right] = \left[\frac{P}{I}\right]$ ie, [3][$\frac{M}{4}$] = $\frac{F}{1}$ = $\frac{F}{13}$ but, [B][M][L] = [B][\frac{1}{7}] = [B] = [1]

<u>Part II</u>. Work out the answer in the space provided. Show details of your work and clearly identify your answer. Grading will be on the basis of approach and answers.

5. The equation shown below is the Darcy equation for radial, horizontal flow of a real gas for pressures where the μz product is constant, in Darcy Units.

$$q_{r} = \left(\frac{T_{sc}}{p_{sc}}\right) \left(\frac{2\pi kh}{\mu z T \ln \binom{r_{e}}{r_{w}}}\right) \left(\frac{p_{e}^{2} - p_{w}^{2}}{2}\right)$$

Determine the constant, C and its units, to convert the terms to the following units: q in standard $\rm ft^3/day$, k in md, h in ft, p in psi, μ in cp, and T in oR . Assume standard conditions are 60 oF and 14.73 psia.

C has units (5+d ft /day (cp)(°R) = cp-ft ? °R (mh)(ft)(psi2) = md.day.psi2

d = 11 1.1271×10 gp-bb1 5.61459 A3 (60+459.61) R md.ft.day.ps, bb1 14.73 ps,

= 0,70138 \frac{cp. \partit{g. op}}{md.day.ps.2

6. A reservoir has a thickness of 100.0 feet, a porosity of 0.15, and a formation compressibility of 5.0×10^{-6} psi⁻¹. Assume the formation subsides when the fluid pressure decreases and the bulk volume compressibility is equal to the product of the porosity and the formation compressibility. Determine the subsidence of the top of the formation when the reservoir pressure decreases 2000.0 psi.

$$V_{6} = \phi c_{4} = \frac{1}{V_{b}} \frac{dV_{b}}{dp} = \frac{1}{h} \frac{dh}{dp} \text{ (Since } V_{b} = Ah \text{)}$$
Separating variables and integrating
$$\begin{pmatrix} h(p-2000) \\ dh \\ h \end{pmatrix} = \phi c_{4} \int dp \text{ (assume $6$4 is constant)}$$

$$h(p) \qquad p$$

$$h(p-2000) = h(p)e^{-2000} \phi c_{4} \Rightarrow$$

$$h(p) - h(p-2000) = Ah = h(p) (1-e^{-2000} \phi c_{4})$$

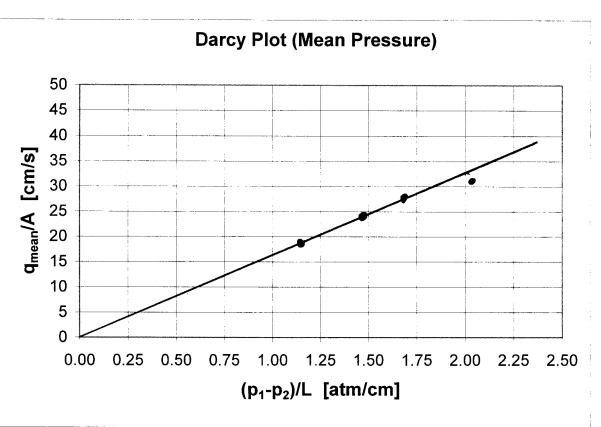
$$= (100)(1-0.995) = 0.15 \text{ ft}$$

7. Using the gas flow data below on a small cylindrical sample, determine the absolute permeability by plotting the appropriate terms of the mean pressure form of Darcy's Law. A blank graph format is provided for the plot. The downstream pressure is atmospheric.

$$\overline{q} = \frac{k A}{\overline{\mu}_g L} \left(p_1 - p_2 \right)$$

Atmospheric	Sample	Sample	Gas Viscosity
Pressure,	Length,	Diameter,	(at mean pressure),
atm	in	in	cp
1.000	1.005	0.995	0.0176

Absolute Upstream pressure, atm	Mean Flow Rate (at mean pressure), cm ³ /s	g/A em/s	P1-P2	
6.23	152	30,3	2.05	
5.34	141	28.1	1.70	
4.75	122	24,3	1,47	
3.90	94.2	18.8	1.14	



Slope =
$$16.5 \frac{\text{cm}^2}{\text{atm.s}} = \frac{k}{\text{Jy}} \Rightarrow k = 0.290 \frac{\text{epcm}^2}{\text{atm.s}}$$

= 0.29 d

8. To determine the matrix volume of a limestone core, a whole core 3.01 inches in diameter and 6.05 inches in length is placed in Cell 2 of a Boyles Law device. Each of the cells has a volume of 1000.0 cm³. Cell 1 is pressured to 50.0 psig and Cell 2 is evacuated. The cells are connected and the resulting pressure is 28.1 psig. Assume the atmospheric pressure is 14.5 psia. Determine the porosity of the core.

$$V_{b} = \frac{\pi d^{2}l}{4} = 705,47 \text{ cm}^{3}$$

$$P_{1}V_{1} = P_{2}V_{2}$$

$$V_{2} = \frac{A_{1}}{P_{2}}V_{1} = \frac{(50.0 + 14.5)}{26.1 + 14.5} \frac{p_{51a}}{p_{51a}} (1000) \text{ cm}^{3}$$

$$= 1514.08 \text{ cm}^{3}$$

$$V_{ma} = 2000 - V_{2} = 485.92 \text{ cm}^{3}$$

$$V_{b} = 1 - \frac{485.92 \text{ cm}^{3}}{705.47 \text{ cm}^{3}}$$

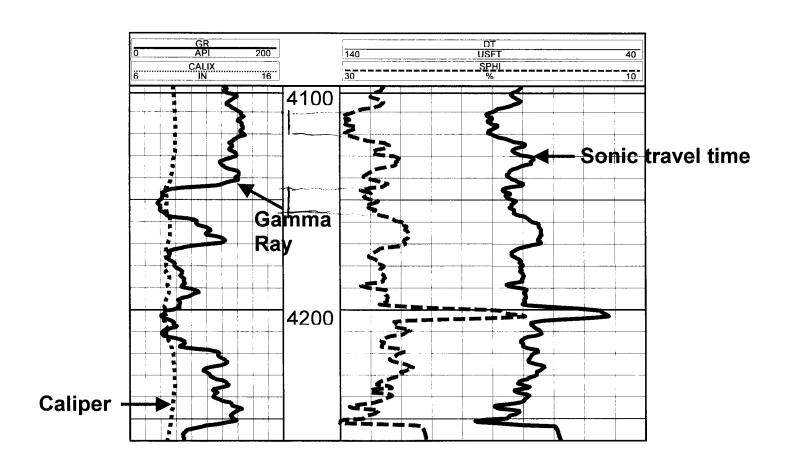
9. a. Determine the readings of the Caliper (CALIX), Gamma Ray (GR), and Sonic Travel Time (DT) Logs at the following intervals:

Interval (feet)	Caliper (inches)	Gamma Ray (API Units)	Sonic Travel Time (μsec/ft)
4110-20	8 in	144 MI	90 Msa/H
4145-55	7.4 in	40 API	84 usa/#

b. Use these readings to determine the porosity at 4245-55 ft, assuming matrix is limestone and the fluid in the pores is water ($\Delta t_{ma} = 47.5 \, \mu sec/ft$, $\Delta t_{f} = 189 \, \mu sec/ft$).

$$\Delta t \log \approx \Phi \Delta t_{f} + (1-b)\Delta t_{ma} = 0.258$$

$$\Phi = \frac{\Delta t_{g} - \Delta t_{ma}}{\Delta t_{f} - \Delta t_{ma}} = \frac{84 - 47.5}{185 - 47.5} = 0.258$$



10. Consider the following whole core analysis data.

		Horizontal	Vertical	
Sample	Depth	Permeability	Permeability	Porosity
Number	(ft)	(md)	(md)	(fraction)
96	9131.5- 32.0	35.9	119.	0.166
97	9132.0-33.0	46.7	304.	0.179
98	9133.0- 34.0	27.8	22.1	0.154
99	9134.0- 35.0	15.1	12.9	0.132
100	9135.0- 36.0	4.61	2.94	0.118
101	9136.0- 37.0	25.5	92.5	0.169

Determine the average horizontal permeability, the average vertical permeability, and the average porosity of these data.

$$\frac{k_h}{h} = \frac{2k_h}{h} = \frac{137.86 \text{ mdft}}{5.5 \text{ pt}} = \frac{25.0 \text{ md}}{5.00 \text{ md}} \quad (260)$$

$$\frac{hv}{h} = \frac{L}{\frac{L}{K}} = \frac{5.5 \text{ ft}}{0.4812 \text{ md}} = \frac{11.4 \text{ md}}{11.3}$$

$$\phi = \frac{5 \phi h}{h} = \frac{0.835 \, ft}{5.5 \, ft} = \frac{0.152}{0.153}$$