

PROBLEM # 1

Refer to Example 2-8 and Figure 2-32 on page 75-76 of ABW. Assume that the solids removed during filtering alter the permeability of the bed and that the alteration is reversal, making it necessary to remove the solids periodically by reversing the flow; that is, by flowing the water vertically upward through the bed. What head of water is required to remove the solids if the reverse flow rate is (a) 5000 gallons/hr, and (b) 1000 gallons/hr?

THEORY

$$\frac{q_s}{A} = -\frac{k}{\mu} \left(\frac{dp}{ds} - \rho g \frac{dz}{ds} \right), \quad z^+ \downarrow$$

SOLUTION

comparison of Eqs. 2-23 and 2-2v

$$q = \frac{kA}{\mu} \rho g \left(\frac{h}{L} + 1 \right) \downarrow \quad \text{and} \quad q = \frac{kA}{\mu} \rho g \left(\frac{h}{L} \right) \uparrow$$

a) Using the data of Ex 2-8, the value of $\left(\frac{h}{L} \right)$ for upward flow is 2.72 or

$$\frac{h}{L} = 2.72 \Rightarrow \underline{h = 10.9 \text{ ft}}$$

b) when the rate is 1000 gallons/hr

$$\frac{h}{L} = (0.2)(2.72) = 0.54 \Rightarrow \underline{h = 2.18 \text{ ft}}$$

CHECK

$$\left(\frac{h}{L} \right) = \frac{q \mu}{k A \rho g} = \frac{5000 \text{ gal/hr} \cdot 1 \text{ cp} \cdot 1}{1 \text{ g/cm}^3 \cdot 1.2 \text{ d} \cdot 980 \text{ cm/s}^2 \cdot \text{dyne}} \cdot \frac{1.01325 \times 10^6 \text{ dyne/cm}^2}{\text{atm}} \cdot \frac{3785.4 \text{ cm}^3}{\text{gal}} \cdot \frac{\text{hr}}{3600 \text{ s}} \cdot \frac{\text{ft}^2}{(30.48)^2 \text{ cm}^2} = 2.70885$$



PROBLEM # 2

Derive an equation for horizontal, radial flow of an incompressible liquid from a general radius r to the radius of the wellbore, $r = r_w$. List the assumptions made. Graph the pressure at a general radius r , as a function of radius ($r = 0.1$ to 1000 m). For graphing purposes, assume $q\mu/(2\pi kh) = 5.0$ atmospheres and the flowing pressure at the wellbore is 50 atmospheres. What do you conclude from your graph?

THEORY

$$\frac{q_s}{A} = -\frac{k}{\mu} \left(\frac{dp}{ds} - \rho g \frac{dz}{ds} \right), \quad z^+ \downarrow$$

SOLUTION

1) Assumptions

- Darcy's Law (Darcy flow, ss flow, non-reactive fluid, single phase ($S=1$))
- PVT (incompressible liquid, isothermal conditions)
- Geometry (radial flow, $ds = -dr$, $A = 2\pi rh$ (h const), $\frac{dz}{ds} = 0$)

$$2) \quad v_s = \frac{q_s}{A} = -\frac{k}{\mu} \left(\frac{dp}{ds} - \rho g \frac{dz}{ds} \right)$$

$$q_r = 2\pi r h \frac{k}{\mu} \frac{dp}{dr}$$

3) Separate variables & integrate

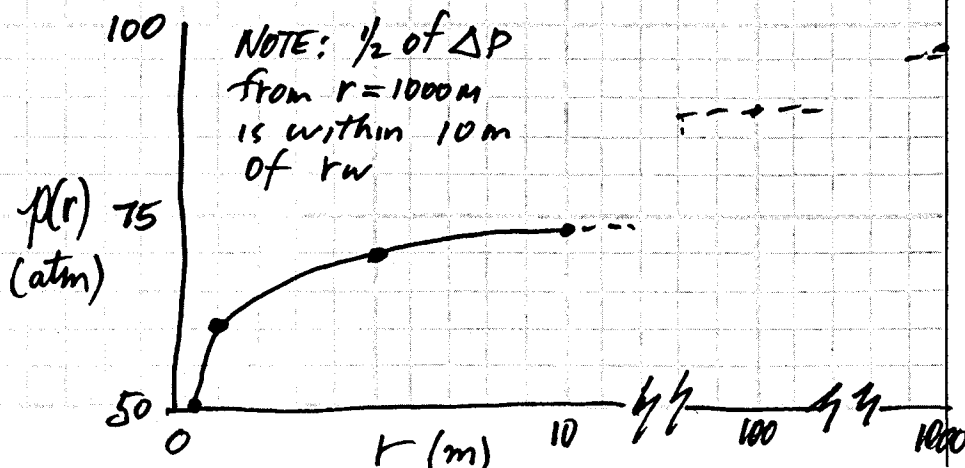
$$r_w \rightarrow r, \quad p_w \rightarrow p(r)$$

$$q_r \int_{r_w}^r \frac{dr}{r} = \frac{2\pi r h}{\mu} \int_{p_w}^{p(r)} dp \Rightarrow p(r) = p_w + \frac{q_r \mu}{2\pi r h} \ln\left(\frac{r}{r_w}\right)$$

4)

r	$p(r)$
$0.1 = r_w$	50
1	61.5
10	73.0
100	84.5
1000	96.1

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spe

PROBLEM # 3

Calculate real gas pseudopressure at a pressure of 1902.7 psia using the following data and a base pressure of 102.7 psia. Was the calculation of real gas pseudopressure necessary for this gas? Explain your answer.

p (psia)	z	μ_g (cp)
1902.7	0.87155	0.0164
1602.7	0.88030	0.0153
1302.7	0.89426	0.0144
1002.2	0.91298	0.0136
702.7	0.93565	0.0129
402.7	0.96155	0.0123
102.7	0.98987	0.0120

THEORY

$$m(p) = 2 \int_{p_b}^p \frac{p}{\mu z} dp$$

SOLUTION

pressure psia	z-factor	viscosity cp	μz cp	$2p/\mu z$ psia/cp	Area psia ² /cp	m(p) psia ² /cp
1902.7	0.87155	0.0164	0.0143	2.66E+05	7.56E+07	2.78E+08
1602.7	0.88030	0.0153	0.0135	2.38E+05	6.60E+07	2.03E+08
1302.7	0.89426	0.0144	0.0129	2.02E+05	5.47E+07	1.37E+08
1002.2	0.91298	0.0136	0.0124	1.61E+05	4.16E+07	8.21E+07
702.70	0.93565	0.0129	0.0121	1.16E+05	2.77E+07	4.05E+07
402.70	0.96155	0.0123	0.0118	6.81E+04	1.28E+07	1.28E+07
102.70	0.98987	0.0120	0.0119	1.73E+04	0.00E+00	0.00E+00

Note that $\mu z \approx \text{constant} = 0.0131 \text{ cp}$ and

$$\int_{p=102.7}^{p=1902.7} \frac{2p}{\mu z} dp \approx \frac{2}{0.0131} \left[\frac{(1902.7)^2 - (102.7)^2}{2} \right]$$

$$= 2.76 \times 10^8 \text{ psia}^2/\text{cp}$$

CONCLUSION

$$m(1902.7) = 2.78 \times 10^8 \text{ psia}^2/\text{cp}$$

Not necessary in this case because $\mu z \approx \text{constant}$



PROBLEM # 4

Find the required constant and its units to convert the Darcy equation for linear, horizontal flow

$$q = \frac{kA\Delta p}{\mu L}$$

to the following unit system ($q, k, L, A, \Delta p, \mu$): liters per minute, millidarcy, centimeters, centimeters squared, dynes/square centimeter, and centipoise.

THEORY

Convert the units of the "hidden constant"

SOLUTION

"1" has units $\frac{\text{cp} \cdot \text{cm}^2}{\text{d} \cdot \text{atm} \cdot \text{s}}$

$$\frac{1 \text{ cp} \cdot \text{cm}^2}{\text{d} \cdot \text{atm} \cdot \text{s}} \cdot \frac{\text{d}}{10^3 \text{ md}} \cdot \frac{\text{atm}}{1.01325 \times 10^6 \text{ dynes/cm}^2} \cdot \frac{\text{cm}}{\text{cm}} \cdot \frac{\text{liter}}{10^3 \text{ cm}^3} \cdot \frac{60 \text{ s}}{\text{min}} =$$

$$\underline{\underline{5.9215 \times 10^{-11} \frac{\text{cp} \cdot \text{liter}}{\text{md} \cdot \text{dynes/cm}^2 \cdot \text{min} \cdot \text{cm}}}}$$

